



NEP Mission Performance Technology Drivers

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NEP Mission Performance Technology Drivers



- NASA/MSFC Lead NEP Tiger Team II Vehicle Concept Starting Point
We have to understand where we are in order to determine what technology advances are necessary!
- Technology Assumptions for Improved Performance
- Sensitivity of Neptune/Triton Mission Trip Times to
 - Decreased Dry Mass
 - Increased Thruster Efficiency
 - Increased Power
- The Physics Behind the Results
- Specific Electric Propulsion System Technology Challenges

JPL Nuclear Electric Propulsion Tiger Team II



Team Members



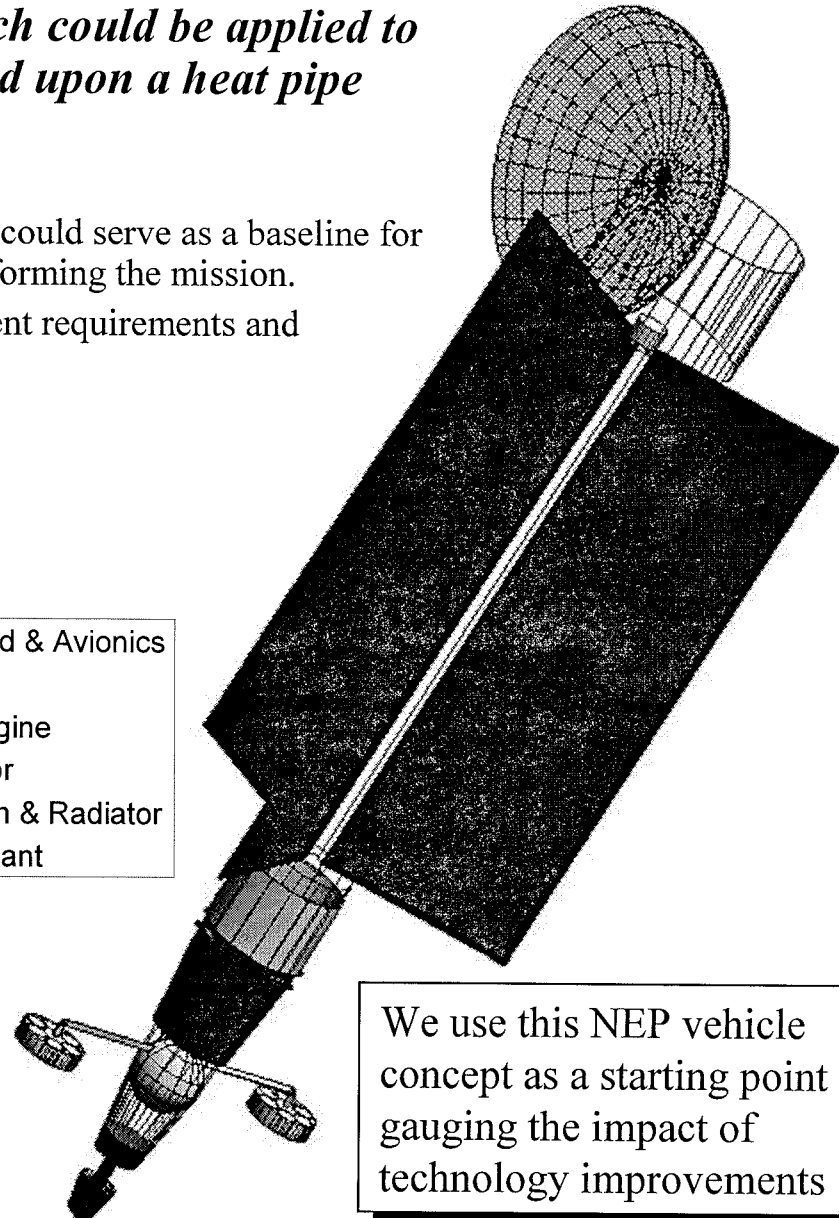
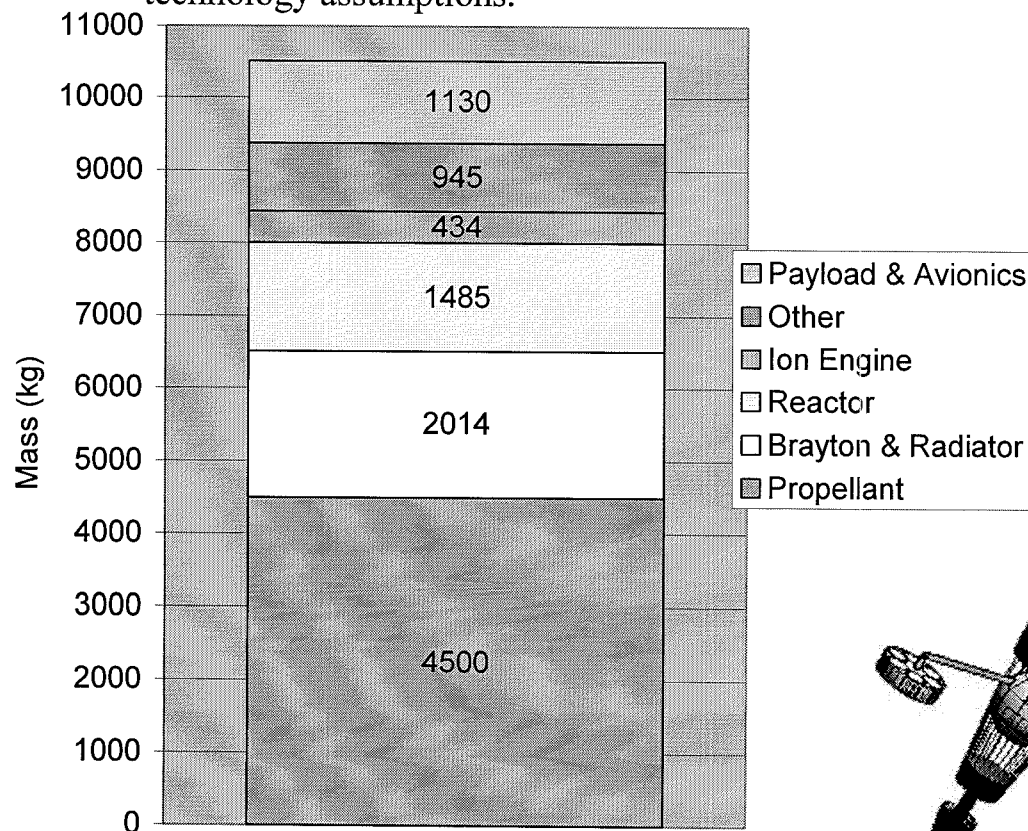
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An NEP spacecraft “point design”, which could be applied to future trade studies, was generated based upon a heat pipe reactor, Brayton cycle and ion engines.

Key Study Highlights

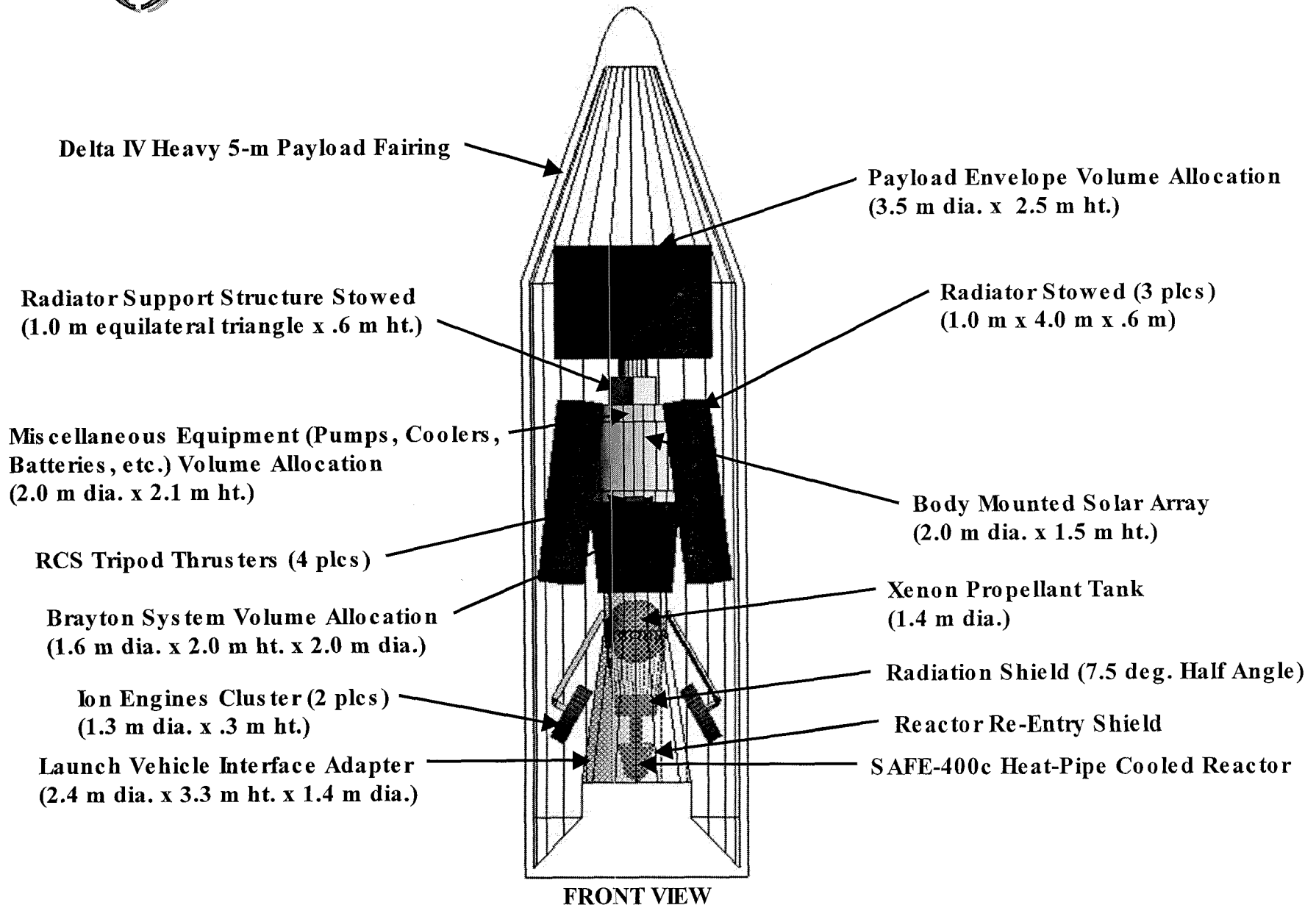
1. This is a non-optimized spacecraft design that could serve as a baseline for future trade studies and has the potential of performing the mission.
2. Meeting the mass goal is difficult with the current requirements and technology assumptions.



We use this NEP vehicle concept as a starting point for gauging the impact of technology improvements



Stowed Conceptual Configuration





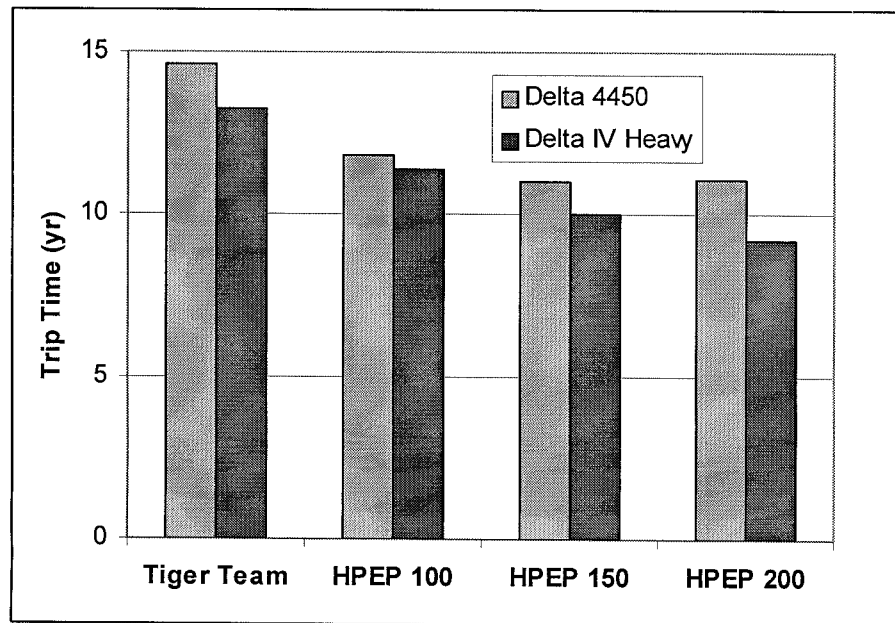
High Power & Technology Improvements Needed to Achieve 10 Year HPEP Missions



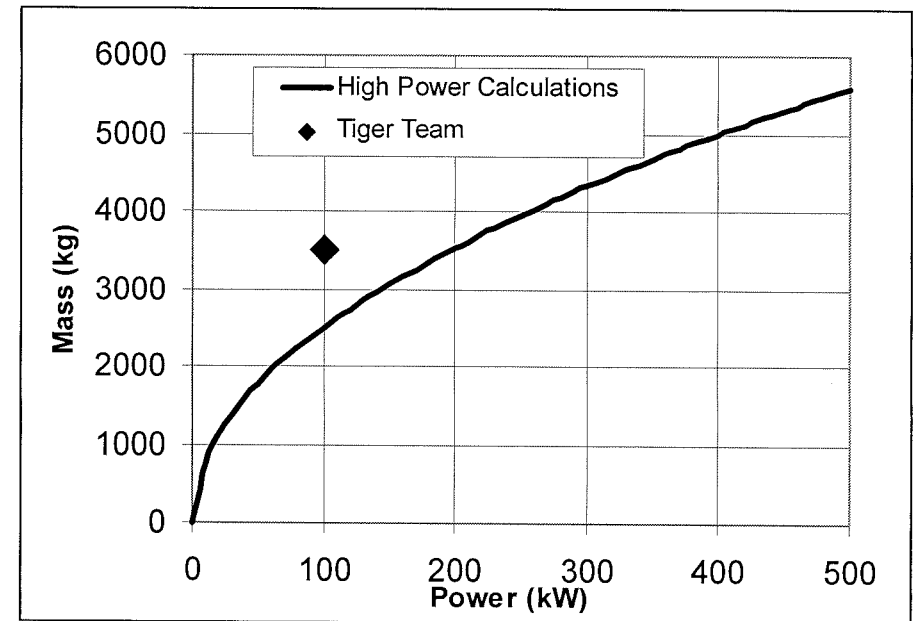
- Mission: Triton/Neptune
- Tiger Team Vehicle 14.6 Years
- 3 Approaches to Improved Trip Time
 - Power technology - reduced mass
 - Thruster efficiency
 - Higher power (square root scaling)
- All 3 needed to Achieve 10 Year Mission

Vehicle Assumptions

	Tiger Team	HPEP 100	HPEP 150	HPEP 200
Power	100	100	150	200
Power Mass	3500	2500	3062	3536
Total Dry Mass	5500	4500	5400	6160
Thruster Eff	73%	80%	80%	80%
PPU Eff	95%	95%	95%	95%
Efficiency	69%	76%	76%	76%
Trip Time (yr)				
Delta 4450	14.6	11.8	11.0	11.1
Minimum	13.3	11.4	10.0	9.2



Triton/Neptune Mission



Power System Mass



Technology Steps to Improve Performance



Technology choices that get us from:
3500kg/73% → 2500kg/80%

- Tiger Team System

Reactor

Heat pipe with 3 exchangers

Reactor 650 kg

Heat Exchangers 213 kg

Power Conversion System

Three 40 kw Brayton system

Mass (inc. radiators) 2014 kg

Ion Engines

Xenon with individual
neutralizers

Engine efficiency < 73.5%

Dec Tiger Team presentation

- HPEP System

Reactor

Gas Cooled Reactor

Mass saving ~163 kg

My estimate, no inputs

Power Conversion System

Single 100 kw Brayton system

Mass saving ~800 kg

Extrapolating GRC converter size trade study in Tiger Team final report that showed ~ 400kg saving going from 3 to 2.

Ion Engines

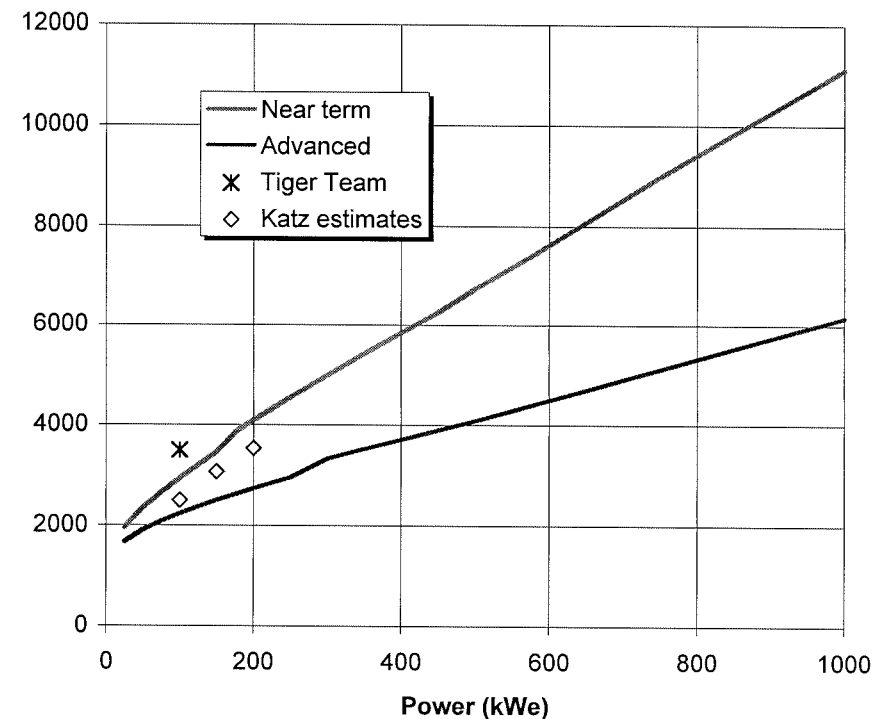
Single neutralizer for multiple engines ~
3-4% improvement

Has been demonstrated in laboratory test.
Theory of space operation is being
validated with DS1 flight data.

Improved discharge chamber propellant
utilization ~ 3-4% improvement

Competition sensitive new technology
concept based on validated computer
code simulations

- Tiger Team Design Point
 - 3x35 kWe Brayton Engines
 - 1144 K Turbine Inlet Temperature
 - 25% System Efficiency
 - SAFE Heat Pipe Reactor + HSHX (1535 kg)
- Near Term Power Curve
 - 2 Brayton Engines at 50% Power
 - 1150 K Turbine Inlet Temperature
 - 21 to 24% System Efficiency
 - Liquid Metal Cooled Reactor (Scaled SP-100)
- Advanced Power Curve
 - 2 Brayton Engines at 50% Power
 - 1500 K Turbine Inlet Temperature
 - 30 to 34% System Efficiency
 - Liquid Metal Cooled Reactor (Scaled SP-100)



(Bob Cataldo & Lee Mason)

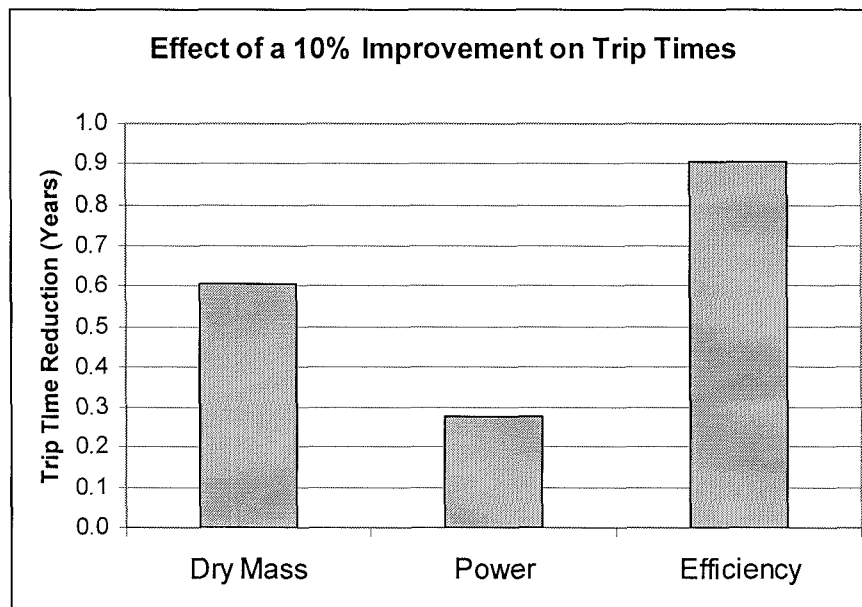
- Baseline Assumptions:

Payload	500kg
Power	3500kg
Propulsion	500kg
Other	1000kg
PPU Efficiency	95%
Thruster Efficiency	73%
Tankage + Margin	20%

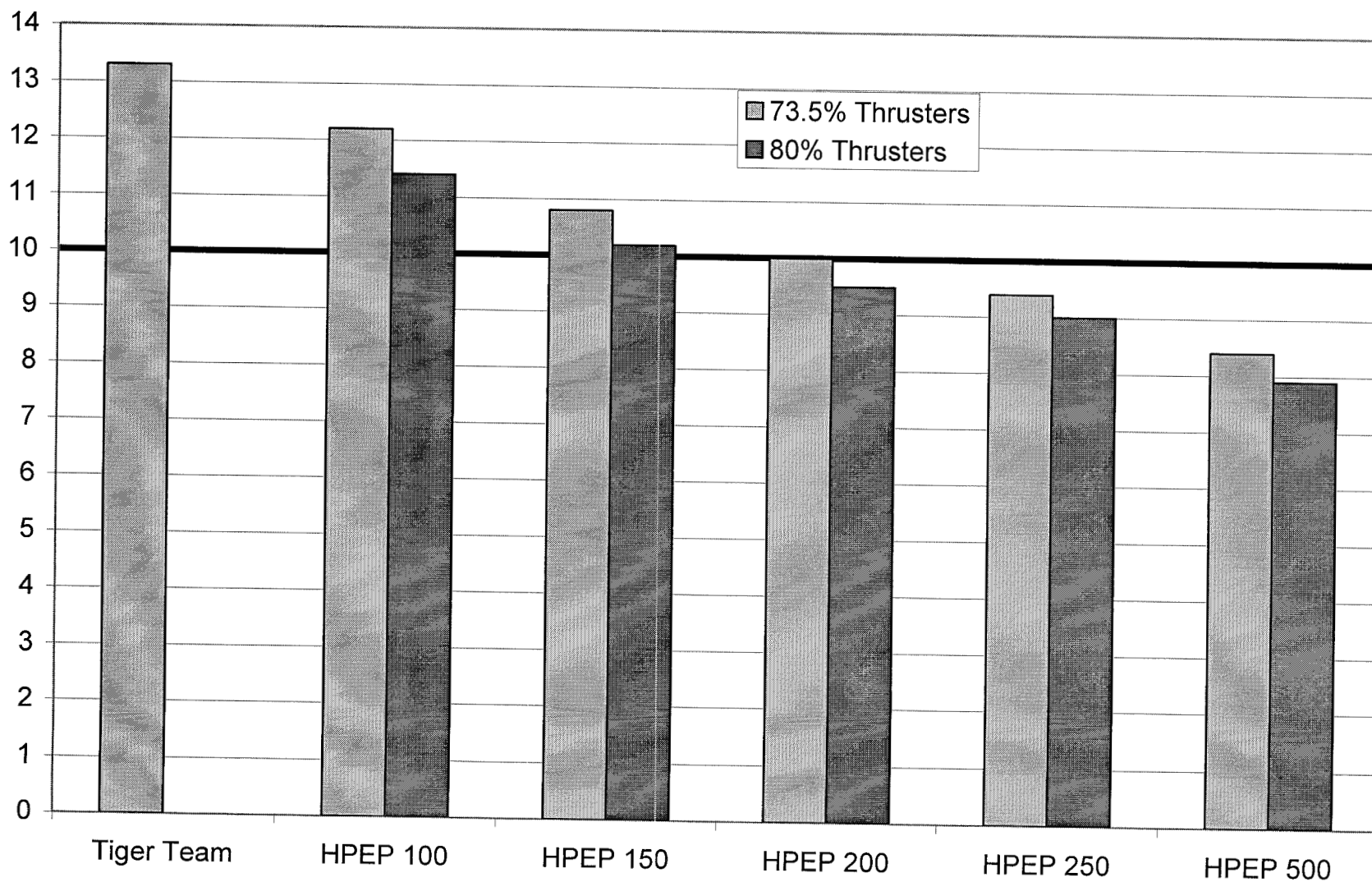
- Enhanced Systems

Reduced power system mass

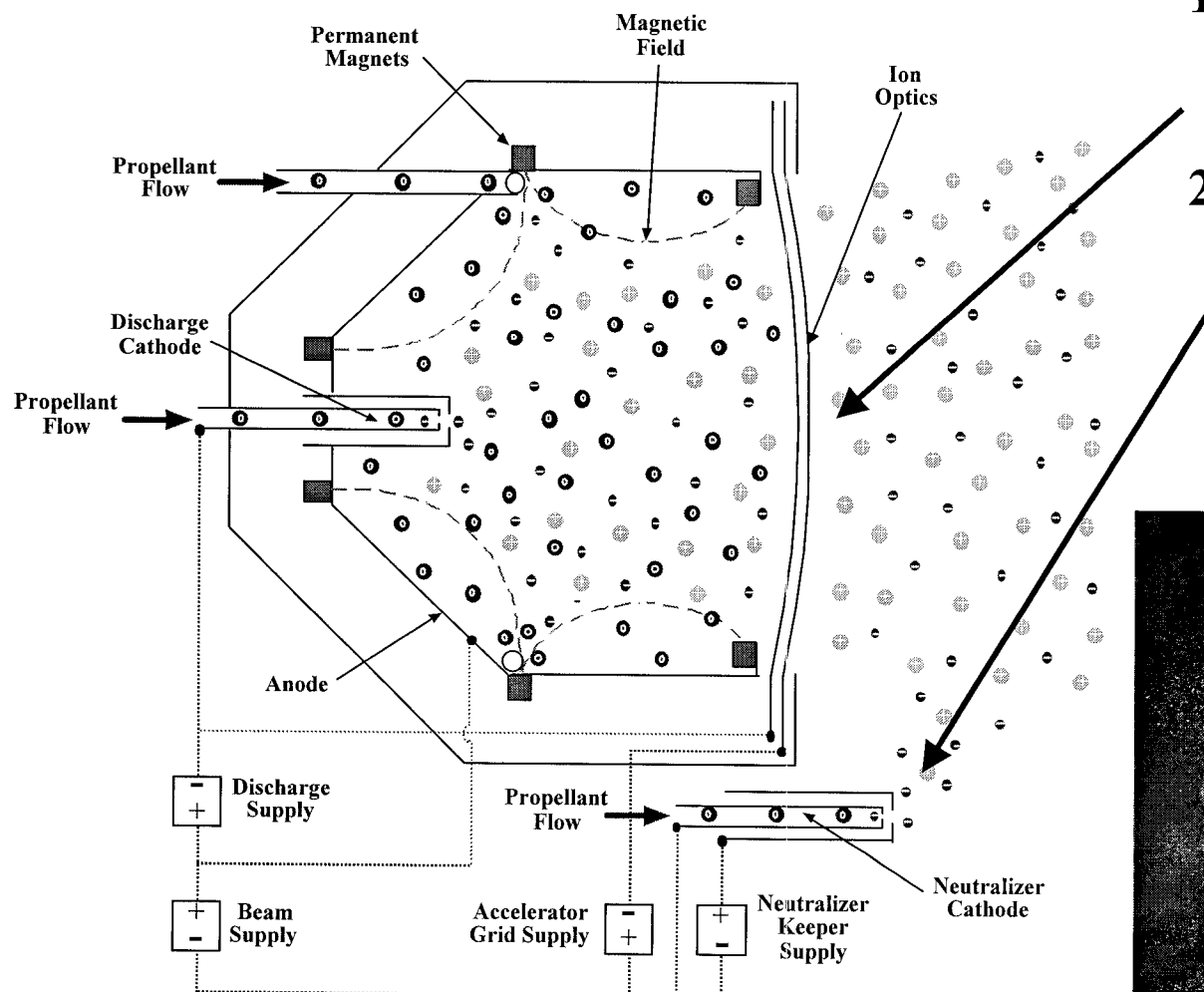
All masses except Payload scale with square root of Power



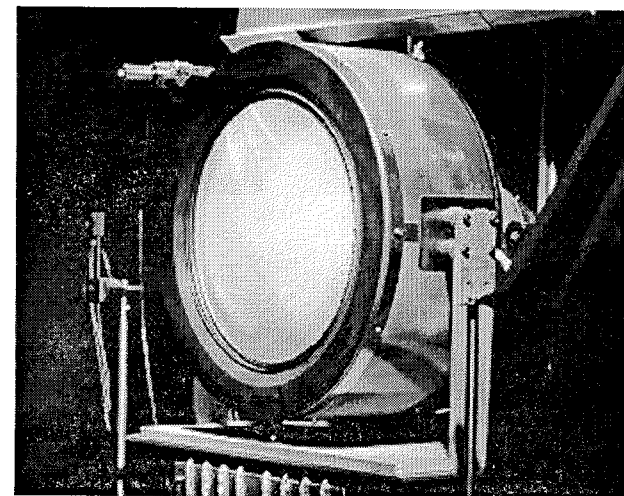
	Tiger Team	HPEP 100	HPEP 150	HPEP 200	HPEP 250	HPEP 500
Power	100	100	150	200	250	300
Power Mass	3500	2500	3062	3536	3953	4330
Total Dry Mass	5500	4500	5400	6160	6825	9440
PPU Eff	95%	95%	95%	95%	95%	95%
Thruster Eff	73.5%	73.5%	73.5%	73.5%	73.5%	73.5%
Efficiency	70%	70%	70%	70%	70%	70%
Trip Time (yr)						
Delta 4450	14.6	12.6	11.4	11.6	11.6	11.6
Delta IV Heavy	13.3	12.2	10.8	10.0	9.4	8.4
Thruster Eff		80.0%	80.0%	80.0%	80.0%	80.0%
Efficiency	0%	76%	76%	76%	76%	76%
Trip Time (yr)						
Delta 4450		11.7	11.0	11.0	11.2	
Delta IV Heavy		11.4	10.2	9.5	9.0	7.9



How Propellant Escapes From Ion Thrusters



1. Unionized gas escapes through holes in the grids
2. Ions and neutral gas come out of the hollow cathode neutralizer



Engineering model ion thruster built by NASA GRC during 8200 hour endurance test at JPL.



Propellant Utilization Helps Performance



- Newton's second law describes NEP vehicle motion

$$m\mathbf{a} = \mathbf{F}$$

$$m \frac{d\mathbf{v}}{dt} = \dot{m} \bar{\mathbf{v}} = \dot{m} (f_{beam} \mathbf{v}_{beam} + (1 - f_{beam}) \mathbf{v}_{gas})$$

$$\approx \dot{m} f_{beam} \mathbf{v}_{beam}$$

- If we consider dry mass and propellant masses, we can integrate to get the rocket delta v

$$m \frac{dv}{dt} = \frac{dm}{dt} f_{beam} v_{beam}$$

$$\int_{v_0}^{v_f} \frac{dv}{f_{beam} v_{beam}} = \int_{m_{dry} + m_{prop}}^{m_{dry}} \frac{dm}{m}$$

$$\Delta v = f_{beam} v_{beam} \ln \left(1 + \frac{m_{prop}}{m_{dry}} \right)$$

NOTE: Δv is proportional to propellant utilization, f_{beam}

Trip Times Decrease Slowly With Increased Power

- Time is roughly proportional to the square root of the acceleration

$$\mathbf{a} \approx \frac{\dot{m} f_{beam} \mathbf{v}_{beam}}{m}$$

$$t_{trip} \propto \sqrt{\frac{m}{f_{beam}}}$$

Same Dependence on Mass, Propellant Utilization

- For a fixed I_{sp} , the thrust is proportional to the beam power

$$P_{beam} = \frac{1}{2} \dot{m} f_{beam} v_{beam}^2$$

- If the mass increases with the square root of the power

$$\mathbf{a} \propto \frac{P}{m}$$

$$t_{trip} \propto \sqrt{\frac{m}{P}}$$

$$t_{trip} \propto \frac{1}{P^{1/4}}$$



Requirements for 10 Year Neptune Orbiter Trip



- Back of the envelope estimate

distance	30 AU 4.5E+09 km
time	10 years 3.3E+08 seconds
v average	14 km/s
delta v	54 km/s

- We assume burn time is 2/3 of trip time & rest of system is 88% efficient
- 100 kW system inconsistent with 10 yr trip time

Assumed Power (kW)	100	100	100	100
Dry Mass (kg)	5,500	5,500	4,500	4,500
Launch Mass (kg)	14,000	14,000	11,250	11,250
Propellant Utilization	80%	90%	80%	90%
Required Power (kW)	168	133	137	109

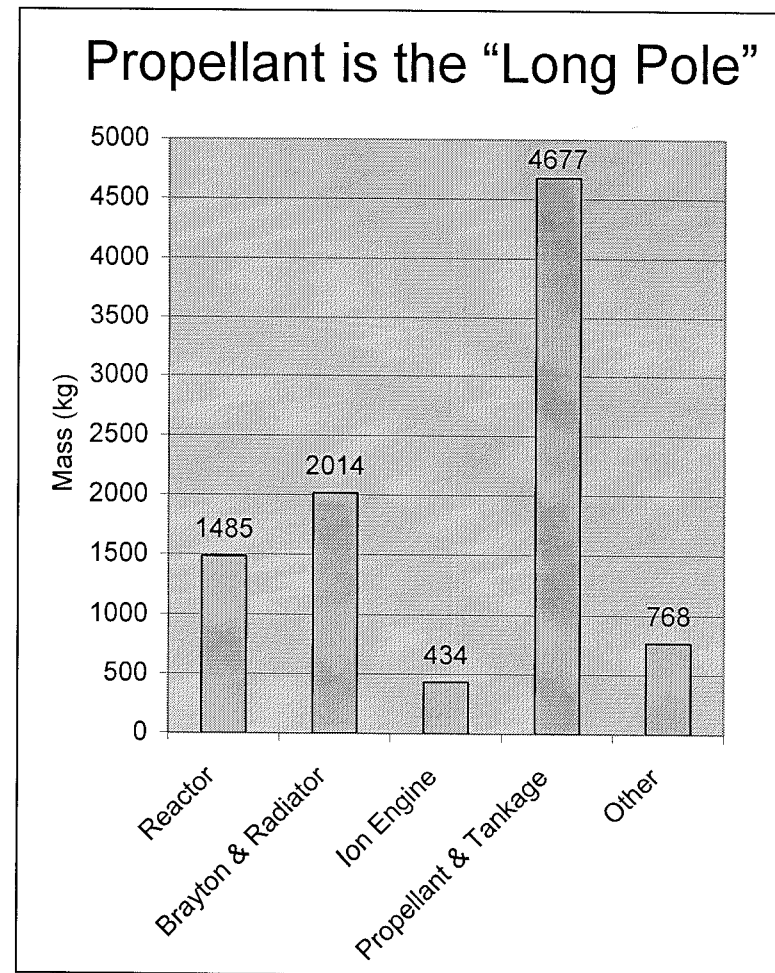
- Improved utilization & higher powers necessary

100kW Dry Mass	5,500	5,500	4,500	4,500
Propellant Utilization	80%	90%	80%	90%
Break Even Power	300	225	200	150
Launch Mass	24,000	21,000	16,000	14,000

JPL Electric Propulsion System Technology Advances That Would NEP Improve Performance



<u>Subsystem</u>	<u>Potential Mass Saving</u>
• Propellant utilization	
Reducing discharge chamber propellant losses by tailoring grid holes to local beamlet diameters	~4% of propellant ~ 200 kg
Single neutralizer for several engines	~4% of propellant ~ 200 kg
• Propellant management	
Improve precision of flow controller from 3% to 1%	~ 2% of propellant ~ 100 kg
• Propellant tank	
Ultra-light weight Xenon tank, reducing tankage from 6% to 3%	~ 3% of propellant ~ 150 kg
• Engine life	
Long life, erosion resistant, high voltage grids	~ 150 kg
Extended life hollow cathode	



Potential Launch Mass Savings of 500-1000 kg!



NEP Mission Performance Technology Drivers



- Only three ways to improve NEP Vehicle performance
 1. **Reduce dry mass**
 2. **Reduce propellant waste**
 3. **Increase power – take advantage of reactor/power system scaling**
- Electric propulsion system technology advances needed
 - Improved propellant utilization – grids & neutralizers
 - Improved flow control accuracy
 - Ultra-lightweight Xe tanks
 - Increased life high *Isp* grids
 - Increased life hollow cathodes
- Radiator packaging in the launch vehicle shroud identified as the leading impediment to higher power systems